A decomposition heuristics for the container ship stowage problem

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Abstract In this paper we face the problem of stowing a containership, referred to as the Master Bay Plan Problem (MBPP); this problem is difficult to solve due to its combinatorial nature and the constraints related to both the ship and the containers. We present a decomposition approach that allows us to assign a priori the bays of a containership to the set of containers to be loaded according to their final destination, such that different portions of the ship are independently considered for the stowage. Then, we find the optimal solution of each subset of bays by using a 0/1 Linear Programming model. Finally, we check the global ship stability of the overall stowage plan and look for its feasibility by using an exchange algorithm which is based on local search techniques. The validation of the proposed approach is performed with some real life test cases.

1. Introduction and problem definition

In this paper we deal with the ship planning problem. The stowage of a containership is one of the problems that has to be solved on a daily basis by any company which manages a container terminal (Thomas, 1989). In the past stowage plans for containers were performed by the Captain of the ship; today, as a consequence of containerisation, the maritime terminal has to decide the stowage of containers following the instructions coming from the maritime company holding the ship and taking into account different interrelated terminal requirements (see Atkins, 1991).

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Formally, the stowage planning problem, known as the Master Bay Plan Problem (MBPP), consists in determining how to stow a given set C of n containers of different type into a set S of m available locations of a containership, respecting some structural and operational constraints, related to both the containers and the ship; the goal is the minimisation of the loading time of all containers. In fact, while the turnaround time of a ship includes the time for berthing, unloading, loading and departure, the major activities affecting the turnaround time are the unloading and loading processes, and, in particular, loading is the more difficult and sensitive to the efficiency of the operations process (Imai et al., 2002).

In the MBPP each container $c \in C$ must be stowed in a location $l \in S$ of the ship. Note that the l-th location is actually addressed by indices i, j, k representing, respectively: the bay (i), that gives its position related to the cross section of the ship (counted from bow to stern), the row (j), that gives its position related to the horizontal section of the corresponding bay (counted from centre to outside), and the tier (k) that gives its position related to the vertical section of the corresponding bay (counted from bottom to top). We will denote by I, J and K, respectively, the set of bays, rows and tiers of the ship, and by b, r and s their corresponding cardinality.

The objective function is expressed in terms of the sum of time t_{lc} required for loading a container c, $\forall c \in C$, in location l, $\forall l \in S$, such that $L = \sum_{lc} t_{lc}$. However, when two or more quay cranes are used for the loading operations the objective function is given by the maximum over the minimum loading time (L_q) for handling all containers in the corresponding ship partition by each quay crane q, that is $L = \max_{QC}\{L_q\}$, where QC is the set of available quay cranes. Note that the time for handling a container by a quay crane depends, as we will see later, on the row and the tier address in the ship and the type of quay crane used.

The main constraints that must be considered for the stowage planning process for an individual port are related to the structure of the ship and focused on the size, type, weight, destination and distribution of the containers to be loaded.

Size of containers. Usually, as in this paper, set C of containers is considered as the union of two subsets, T and F, consisting, respectively, of 20 and 40 feet containers, such that $T \cap F = \emptyset$ and $T \cup F \equiv C$. Standard locations are generally thought for dry 20 feet containers and referred to as one Twenty Equivalent Unit (TEU) location. Containers of 40 feet (denoted by 40') require two contiguous locations of 20 feet (denoted by 20'). Note that according to a practice adopted by the majority of maritime companies, bays with even number are used for stowing 40' containers and correspond to two contiguous odd bays, that are used for the stowage of 20' containers. Consequently, if a 40' container is stowed in an even bay (for instance bay02) the locations of the same row and tier corresponding to two contiguous odd bays (e.g. bay01 and bay03) are not anymore available for stowing containers of 20'.

Type of containers. Different types of containers can usually be stowed in a containership, such as standard, carriageable, reefer, out of gauge and hazardous.

The location of reefer containers is defined by the ship coordinator (who has a global vision of the trip), so that we know their exact position. This is generally near power points in order to maintain the required temperature during transportation. Hazardous containers are also assigned by the harbour-master's office which authorises their loading. In particular, hazardous containers cannot be stowed either in the upper deck or in adjacent locations. They are considered in the same way as 40' containers. Note that, for the definition of

the stowage plan we consider only dry and dry high cube containers, having exterior dimensions conforming to ISO standards of 20 and 40 feet long, either 8 feet 6 inches or 9 feet 6 inches high and 8 feet depth.

Weight of containers. The standard weight of an empty container ranges from 2 to 3.5 tons, while the maximum weight of a full container to be stowed in a containership ranges from 20–32 and 30–48 tons for 20' and 40' containers, respectively. The weight constraints force the weight of a stack of containers to be less than a given tolerance value. In particular the weight of a stack of 3 containers of 20' and 40' cannot be greater than an a priori established value, say MT and MF respectively. Moreover, the weight of a container located in a tier cannot be greater than the weight of the container located in a lower tier having the same row and bay and, as it is always required for security reasons, both 20' and 40' containers cannot be located over empty locations.

Destination of containers. A good general stowing rule suggests to load first (i.e. in the lower tiers) those containers having as destination the final stop of the ship and load last those containers that have to be unloaded first.

Distribution of containers. Such constraints, also denoted stability constraints, are related to a proper weight distribution in the ship. In particular, we have to verify different kinds of equilibrium, namely: (a) horizontal equilibrium, that is the weight on the right side of the ship, including the odd rows of the hold and upper deck, must be equal (within a given tolerance, say Q_1) to the weight on the left side of the ship; (b) cross equilibrium, that is the weight on the stern must be equal (within a given tolerance, say Q_2) to the weight on the bow; (c) vertical equilibrium, that is the weight on each tier must be greater or equal than the weight on the tier immediately over it. Let us denote by L and R, respectively, the set of rows belonging to the left /right side of the ship and by A and P, respectively, the sets of anterior and posterior bays of the ship. In Sections 5 and 6 we will see how the horizontal ship stability constraint impacts on the total loading time by increasing the optimal value.

The description of the entire problem in the form of an optimisation problem is given in Ambrosino et al. (2004).

The MBPP is a NP-complete combinatorial optimisation problem (see. e.g. Avriel et al. (2000) that connect the MBPP to the colouring of circle graphs problem).

Many interesting approaches for solving container loading problems that have some commonalties with the MBPP have been presented in the recent literature (see, e.g., Bischoff and Mariott (1990), Bischoff and Ratcliff (1995), Bortfeldt and Gehring (2001), Davies and Bischoff (1999), Eley (2002), Gehring et al. (1990), Gehring and Bortfeldt (1997) among others).

The first attempt to derive some rules for determining good container stowage plans is reported in Ambrosino and Sciomachen (1998), where a constraint satisfaction approach is used for defining and characterising the space of feasible solutions. Wilson and Roach (1999, 2000) divide the container stowage process into two sub-processes, at a strategic and tactical planning level, respectively. In particular, they use branch and bound algorithms for solving the problem of assigning generalized containers to a bays' block in a vessel; in the second step they find a detailed plan which assigns specific positions or locations in a block to specific containers by a tabu search algorithm. Wilson et al. (2001) present a computer system for generating solutions for the decomposed stowage pre-planning problem illustrated in a case study, using a genetic algorithm (GA) approach in order to generate automatically strategic stowage plans and explore the application of artificial intelligence to cargo stowage problems.

Dubrovsky et al. (2002) use a GA for minimizing the number of container movements in the stowage planning problem, while being able to include with appropriate constraints some ship stability criteria; the authors significantly reduce the search space using a compact and efficient encoding scheme.

Avriel and Penn (1993) and Avriel et al. (1997) focus on stowage planning considering the problem of minimising the number of unproductive shifts (temporary unloading and reloading of container at a port before their destination ports in order to access containers below them for unloading). Martin et al. (1988) develop a heuristic algorithm that in solving the planning problem takes into account the transtainer quay cranes, with the aim of minimising their global longitudinal movement time and the total number of shifts in the successive ports. Sciomachen and Tanfani (2003) present a heuristic method for the MBPP based on its connection to the three dimensional bin packing problem.

Integer Linear Programming models for solving the MBPP have been proposed in Botter and Brinati (1992) and Imai et al. (2002); however, due to many simplified assumptions, they are not suitable for real life large scale applications. Ambrosino et al. (2004) give a 0/1 Linear Programming model and solve it by performing a preprocessing heuristic algorithm.

Here, we present a three phase algorithm for defining stowage plans with the aim of minimising the total loading time of the containers on the ship and satisfying weight, size and stability constraints, related to weight' distribution. In the first phase, denoted main branching tree, we split the ship into different portions and associate containers with different subsets of bays without specifying their actual position. Successively, we find the optimal way for loading containers into each partition of the ship by solving a 0/1 Linear Programming model. Note that in this way the search for the location of each container is limited to a portion of the ship and therefore the space of the solutions is reduced. Finally, we check and remove possible unfeasibilities of the global solution due to the cross and horizontal stability of the ship by performing some local search exchanges.

Note that in the present approach we assume that the ship starts its journey in the port for which we are studying the problem, and successively visits a given number of other ports where only unloading operations are allowed, that is we are only concerned with the loading problem at the first port. However, note that in all the following ports visited by the ship the same loading process holds provided that only the available locations would be considered. Moreover we assume that the number of containers to load on board is not greater than the number of available locations; this means that we are not concerned with the problem of selecting some containers to be loaded among all, and we will verify a priori the capacity of the ship related to the maximum weight and size available for all containers to be loaded.

The proposed bay assignment algorithm is described in Section 2; Section 3 reports the 0/1 Linear Programming model related to each portion of the ship; Section 4 describes how we make the overall solution feasible with respect to the stability conditions of the ship. An application of our algorithm is given in Section 5 by solving a sample problem step by step, and a validation of the approach based on some real life test cases is reported in Section 6. Finally, some conclusions are given in Section 7.

2. The bay assignment algorithm

In this section we will show how to split set I into different partitions, in order to be able to solve separately the loading problem for each portion of the ship, independently on its stability conditions, that will be verified successively. Other decomposition approaches have

been presented in the literature with the same aim of reducing the complexity of the overall problem (Wilson and Roach, 1999, 2001).

The bay partitioning procedure proposed here is based on a main branching tree, consisting of the following four steps. In particular, our bay assignment algorithm can be applied when $b \geq 6$; this choice for b allows at least two quay cranes working in parallel.

Step 1 (Sorting C). We split set C into p subsets C_h, $h = 1, \ldots, p$, where $p > 1$ is the number of different ports visited by the ship, such that $c \in C_h$ if and only if $d_c = h, \forall h = 1, \ldots, p$, where d_c denotes the destination port of container $c, \forall c \in C$. Note that, as it is also in our referring terminal operative scenario, the number of ports to be visited by a ship is generally $p \leq 10$. Moreover, it is assumed that $p < b$, i.e. the number of bays is usually greater than the number of ports to be visited.

All containers are hence grouped together according to their destination, such that $\bigcup_{h=1,\ldots,p} C_h = C$ and $C_g \cap C_h = \emptyset, \forall h \neq g, h, g = 1, \ldots, p$. Let $h = 1$ denote the first destination of the ship, $h = 2$ the second destination, and so on. We then sort C in such a way that $C_h < C_g$ if and only if $h < g$. Elements belonging to C_1 are hence containers to be unloaded first.

Step 2 (Sizing C_h, $h = 1, \ldots, p$). For each subset of containers C_h, $h = 1, \ldots, p$, we compute the corresponding TEUs, denoted by τ_h; that is τ_h is the number of TEUs corresponding to those 20' and 40' containers that belong to C_h, $h = 1, \ldots, p$.

At the end of this step we hence know the size of each subset of containers C_h, $h = 1, \ldots, p$.

Step 3 (Partitioning I). We associate subset C_h, $h = 1, \ldots, p$, with bays $i \in I$, depending on the value of p and the size of C_h, and generate subset I_{C_h} of all bays devoted to the stowage of container $c, \forall c \in C_h$. Let $N(I_{C_h})$ be the number of TEUs belonging to I_{C_h}.

In particular, we first assign the central bay of the ship, namely bay $\lceil b/2 \rceil$, to C_1, where $\lceil b/2 \rceil$ denotes the smallest integer number greater than $b/2$ and C_1 is the subset of containers to be unloaded first; consequently, we initialise $I_{C_1} = \{\lceil b/2 \rceil\}$ and compute $N(I_{C_1})$.

At each decision node of the main branching tree the feasibility of the assignment is checked as follow. If τ_1, that is the number of TEUs of the containers belonging to C_1, is less, within a given TEUs tolerance, than $N(I_{C_1})$, the assignment is accepted, since no further bay is required for loading the whole set C_1. In this case, we start with the search of the bays for loading containers belonging to C_2; otherwise, we assign to C_1 also bay $(\lceil b/2 \rceil + 3)$, update $I_{C_1} = \{\lceil b/2 \rceil, (\lceil b/2 \rceil + 3)\}$ and $N(I_{C_1})$, and check the feasibility of the assignment. If τ_1 is still greater than $N(I_{C_1})$ we go ahead by adding to I_{C_1} bay $(\lceil b/2 \rceil - 3)$ in the left side. In the search for feasibility we continuously add, alternatively at their right and left side, the bays that are externals and contiguous to those that have been already chosen, i.e. $(\lceil b/2 \rceil + 4)$, $(\lceil b/2 \rceil - 4)$, $(\lceil b/2 \rceil + 5)$, etc; when there is not any more available bay in the considered direction, we choose the nearest bay to the centre of the ship, until $N(I_{C_1}) > \tau_1$ and accept the current assignment. We denote by δ_1 the residual number of TEUs belonging to I_{C_1} such that $\delta_1 = N(I_{C_1}) - \tau_1$.

Successively, we assign bay $(\lfloor b/2 \rfloor + 1)$ to C_2, initialise I_{C_2} and check the feasibility of the assignment as before by computing $N(I_{C_2})$; we then jump two or more bays, alternatively, at the right and left side searching for a free bay to assign to C_2. When I_{C_2} is large enough for loading all containers of C_2 the current node is
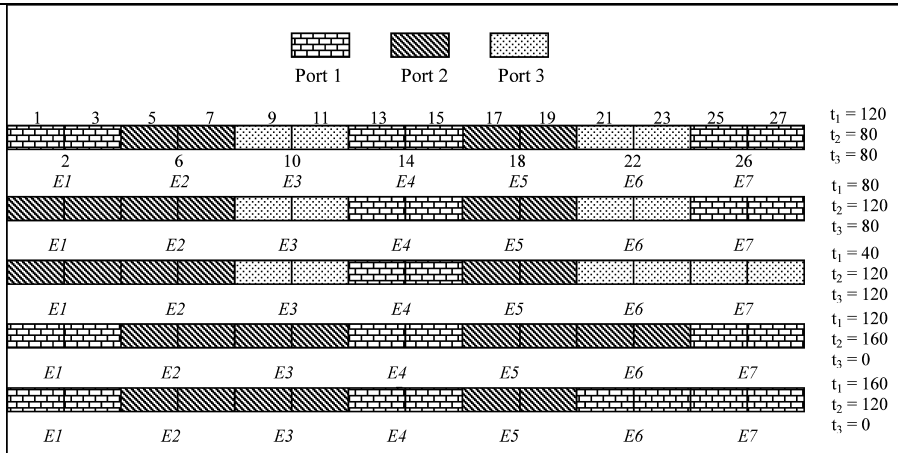
Fig. 1 Examples of different bays' assignments

selected, δ_2 is computed and the bay assignment procedure will proceed considering set C_3, starting from bay $(\lfloor b/2 \rfloor - 1)$ and so on for all existing subsets C_h, $h = 1$, ..., p.

Note that we are not able to know a priori how many bays are required for stowing all containers having the same destination. Moreover, it could occur that for some C_h, $h = 2, \ldots, p$ there are not enough bays for assigning τ_h; then, in this case we look for available locations among the residual δ_{h-1} ones. It will be shown that in all our test cases (see Section 6) each bay is devoted to the stowage of containers of the same destination thus finding a feasible solution of the bay assignment procedure without using any residual δ_h. Some examples of different ways of assigning set of bays to containers are reported in Figure 1, where instances with either 2 or 3 different ports to be visited by a 14 bays hold-ship, with 4 rows and 5 tiers, are given; the number of TEUs of each subset C_h, $h = 1, \ldots, 3$, for the different cases are also given in Figure 1.

Note that this bay assignment procedure is aimed at implementing two operative rules. The first rule suggests that those containers to be unloaded first are located in the central bays in order to avoid as much as possible unbalances in the bow—stern weight distribution after the visit at the first discharging port; moreover, in the bays contiguous to the central ones we locate on one side containers having as destination the second port and on the other those having the third port as final destination, thus avoiding unbalances after the first and the next unloading operations. The second rule is to let two bays between containers with the same destination, thus enabling easier and faster container handling operations; in fact, in a "three transtainers quay complement" two bays between the transtainers are required for letting them work in parallel.

Step 4 (Reducing S for subset C_h, $h = 1, \ldots, p$). We split set S of all m available locations into p subsets S_{C_h}, $h = 1, \ldots, p$, that identify all locations l_{ijk} having as bay address the values corresponding to the bays' assignments defined in Step 3, such that $l_{ijk} \in S_{C_h}$ if and only if $i \in I_{C_h}$, $\forall h = 1, \ldots, p$.

Successively, we remove from S_{C_h}, $h = 1, \ldots, p$, those locations that a priori are not to be considered for stowing container c, $\forall c \in C_h$. In particular, we remove all

locations in odd bays for 40' containers and those in even bays for 20' ones, since they cannot be considered in any feasible solution (see Section 1).

We denote by $\bar{S}_{C_h}$ the set of really available locations for stowing containers belonging to C_h, and by T_h and F_h, the sets of 20' and 40' containers of C_h, respectively, such that $T_h \cup F_h \equiv C_h$. In practice, in this step we initially assign S_{C_h} to $\bar{S}_{C_h}$ and remove from it location l_{ijk} if any of the following conditions is satisfied:

$$if\,(F_h \neq \emptyset)\,then\,for\,(i \in O; c \in F_h; \forall j, k)\bar{S}_{C_h} := \bar{S}_{C_h} \setminus \{l_{ijk}\};$$

$$if\,(T_h \neq \emptyset)\,then\,for\,(i \in E; c \in T_h; \forall j, k)\bar{S}_{C_h} := \bar{S}_{C_h} \setminus \{l_{ijk}\},$$

where O and E denote, respectively, the set of bays with odd and even number.

It can be easily noted that the time complexity of the overall algorithm is bounded by a quadratic polynomial function in the number of bays; in particular, the worst case complexity is $O(pb^2)$ due to Step 3.

3. A 0/1 model for the optimal stowage of each ship partition

The procedure presented above allows us to do not consider the destination constraints that are active combinatorial ones and strongly affect the computational time (Wilson and Roach, 1999). In particular, remember that the destination constraints force containers stowed in the highest tiers to be unloaded first and hence from an operative point of view they are very important; in fact, without considering the unloading port some containers loaded last could be necessarily moved for enabling the unloading operations of some others, thus causing the so called "empty moves" and increasing the turnaround time. Some interesting results based on the reduction of the number of restows and/or empty moves are given in Avriet et al. (1997) and Botter and Brinati (1992), where a binary decision model is given that is explosive in the resolution step; Dubrovsky et al. (2002) use an efficient genetic algorithm for minimizing container movements and, finally, in Imai et al. (2002) stability conditions are given in the objective function of an assignment model together with the minimization of re-handles.

Now we introduce a 0/1 Linear Programming model aimed at finding the optimal way for stowing containers in each partition $\bar{S}_{C_h}$, $h = 1, \ldots, p$, of the ship. Note that by considering only a single partition of the ship, a part from the already mentioned destination constraints, also the cross equilibrium constraints, as they have been described in Section 1, are not included. The decision variables are:

$$x_{ijkc} = \begin{cases} 1 & \text{if in location } l_{ijk} \in \bar{S}_{C_h} \text{ is stowed container } c \in C_h \\ 0 & \text{otherwise} \end{cases}$$

For a better reading of the model we need the following additional notation: w_c, weight of container $c \in C_h$; t_{ijkc}, time for stowing a container $c \in C_h$ in location $l_{ijk} \in \bar{S}_{C_h}$; note that t_{ijkc} includes both the time for lifting container off the quay and the time for putting it into the assigned location.

$$\mathrm{Min} L_{\bar{S}_{C_h}} = \sum_{ijk} \sum_c t_{ijkc} x_{ijkc} \qquad (1)$$

$$\sum_{ijk} x_{ijkc} = 1 \quad \forall c \tag{2}$$

$$\sum_{c} x_{ijkc} \leq 1 \quad \forall i, j, k \tag{3}$$

$$\sum_{c \in T_h} x_{i+1jkc} + \sum_{c \in F_h} x_{ijkc} \leq 1 \qquad \forall i, j, k \tag{4}$$

$$\sum_{c \in T_h} x_{i-1jkc} + \sum_{c \in F_h} x_{ijkc} \leq 1 \qquad \forall i, j, k \tag{5}$$

$$\sum_{c \in T_h} w_c x_{ijkc} + \sum_{c \in T_h} w_c x_{ijk+1c} + \sum_{c \in T_h} w_c x_{ijk+2c} \leq MT \qquad \forall i, j, k = 1, \dots, |K| - 2 \tag{6}$$

$$\sum_{c \in F_h} w_c x_{ijkc} + \sum_{c \in F_h} w_c x_{ijk+1c} + \sum_{c \in F_h} w_c x_{ijk+2c} \leq MF \qquad \forall i, j, k = 1, \dots, |K| - 2 \tag{7}$$

$$\sum_{c} w_c x_{ijkc} - \sum_{c} w_c x_{ijk+1c} \geq 0 \quad \forall i, j, k = 1, \dots, |K| - 1 \tag{8}$$

$$-Q \leq \sum_{i,j \in L, k, c} w_c x_{ijkc} - \sum_{i,j \in R, k, c} w_c x_{ijkc} \leq Q \tag{9}$$

$$x_{ijkc} \in \{0, 1\} \quad \forall i, j, k \forall c \tag{10}$$

(1) is the objective function aimed at minimising the total stowage time of partition $\bar{S}_{C_h}$; it is expressed in terms of the sum of time t_{ijkc} required for loading container c, $\forall c \in C_h$, in location l_{ijk}, $\forall l_{ijk} \in \bar{S}_{C_h}$.

Relations (2)–(3) are the well known assignment constraints forcing each container to be stowed in one ship location and each location to have at most one container.

As we have already said in Section 1, 40' containers can be stowed only in even bays and 20' containers in odd bays; in our model (4) and (5) make unfeasible the stowage of 20' containers in those odd bays that are contiguous to even locations already chosen for stowing 40' containers.

The weight constraints (6) and (7) say that each stack of three 20' and 40' containers cannot exceed some tolerance values MT and MF, respectively, that usually correspond to 45 and 66 tons. Constraints (8) force heavier containers to be put not over lighter ones; (8) also avoid to stow both 20' and 40' containers over empty locations.

Constraint (9) is the horizontal equilibrium requiring that the weight on the right side must be equal, within a given tolerance Q to the weight on the left side of each portion of the ship. Finally, (10) defines the binary decision variables of the problem.

The optimal stowage plan x^* of the whole ship is given by $x^* = \{x^*_{C_1} \cup \dots x^*_{C_h} \dots \cup x^*_{C_p}\}$, where $x^*_{C_h}$ is the optimal solution of model (1)–(10) for ship partition $\bar{S}_{C_h}$, $h = 1, \dots, p$. Note that in Avriel and Penn (1993) a 0/1 Linear Programming model is given for the stowage of a single rectangular bay, knowing in advance, as in our case, the number of containers to be loaded.

If from step 2 of Section 2 we have $\bar{S}_{C_h} \cap \bar{S}_{C_g} \neq \emptyset$ for some $h, g = 1, \dots, p, g < h$, that is, some residual δ_g is used for stowing containers belonging to C_h, then we first solve model (1)–(10) for $\bar{S}_{C_h}$, thus avoiding to load in the lowest tiers of a bay devoted both to C_h and C_g containers to be unloaded first; then, before solving the model for partition $\bar{S}_{C_g}$ we remove

from $\bar{S}_{C_g}$ those locations $l_{ijk} \in \bar{S}_{C_h} \cap \bar{S}_{C_g}$ in which containers belonging to C_h have been already assigned in the optimal solution $x^*_{C_h}$.

It is opportune to observe that following the decomposition approach given in Section 2 we derive the number of bays to assign to each destination port on the basis of the real number of containers to be loaded on board and hence their size and weight are implicitly taken into account also considering the effective given TEUs tolerance (see Section 2); in all our experimentations we never found unfeasible solutions with respect to constraints (2)–(9); however, if an unfeasible solution would be found then the involved containers would be removed from their corresponding partition $\bar{S}_{C_h}$ and put a priory to another one according to the residual TEUs δ_h, $h = 1, \ldots, p$.

Model (1)–(10) has been implemented in MPL and solved for each bay partition up to optimality by using the commercial software CPLEX 7.0 (see Table 3, Section 6). Note that, the unfeasibility due to the horizontal and cross equilibrium of the whole ship will be checked in the last phase of the resolution approach, here below presented. In fact, even if the horizontal equilibrium is satisfied in a partition $\bar{S}_{C_h}$ the global equilibrium of the ship could be violated, as we will see in Sections 5 and 6.

4. An exchange algorithm for the stability conditions

In the last phase we check the stability of the ship and verify both its horizontal and cross equilibrium. In particular, the horizontal stability condition requires, as it has been done with constraint (9) in each portion $\bar{S}_{C_h}$, $h = 1, \ldots, p$, that the weight on the right side must be equal, within a given tolerance Q_1, to the weight on the left side of the ship; the cross stability condition requires that the weight on the stern must be equal, within a given tolerance Q_2, to the weight on the bow. Such conditions can be expressed by constraints (11) and (12):

$$-Q_1 \leq \sum_{i,j \in L,k} \sum_c w_c x^*_{ijkc} - \sum_{i,j \in R,k} \sum_c w_c x^*_{ijkc} \leq Q_1 \tag{11}$$

$$-Q_2 \leq \sum_{i \in A,j,k} \sum_c w_c x^*_{ijkc} - \sum_{i \in P,j,k} \sum_c w_c x^*_{ijkc} \leq Q_2 \tag{12}$$

where x^*_{ijkc} are all variables set to 1 in the optimal solution of partition $\bar{S}_{C_h}$, $h = 1, \ldots, p$.

Let $\eta(x^*)$ be the left-right unbalance, that is the difference between the weight on the left and right side of the ship in the optimal current solution x^*, given by $\eta(x^*) = |\sum_{i,j \in L,k} \sum_c w_c x^*_{ijkc} - \sum_{i,j \in R,k} \sum_c w_c x^*_{ijkc}|$; analogously, let $\chi(x^*)$ be the anterior-posterior unbalance, that is the difference between the weight on the anterior and posterior bays of the ship in the optimal current solution x^*, given by $\chi(x^*) = |\sum_{i \in A,j,k} \sum_c w_c x^*_{ijkc} - \sum_{i \in P,j,k} \sum_c w_c x^*_{ijkc}|$; then, we compute the horizontal and cross stability violations, respectively $\sigma_1(x^*)$ and $\sigma_2(x^*)$, as:

$$\sigma_1(x^*) = \max(\eta(x^*) - Q_1, 0) \tag{13}$$

$$\sigma_2(x^*) = \max(\chi(x^*) - Q_2, 0) \tag{14}$$

Following (13) and (14) the global ship stability unfeasibility is hence given by:

$$\sigma(x^*) = \sigma_1(x^*) + \sigma_2(x^*) \tag{15}$$

We propose some exchanges for making feasible solution x^* obtained at the end of the second phase whenever $\sigma\ (x^*) > 0$, that is if the ship stability is violated. In particular, we change the locations of some containers that are currently stowed in bays belonging to I_{C_h} in order to reduce the unfeasibility value (15) and possibly obtaining a solution that satisfies constraints (11) and (12), without violating constraints of model (1)–(10).

    More precisely, we consider side, cross and bay exchanges among containers as they are defined as follows.

Definition 1. In a *side-exchange* a container c belonging to C is moved from its current location $l \in A \cap L$ (or, analogously $l \in A \cap R$) and put in a location, say f, such that $f \in P \cap L(f \in P \cap R)$. f can be either empty or filled with a container $g \in C$; in this last case g is moved from f and put in location l, that is the original location of container c (and vice versa).

    Note that Definition 1 implies that by performing one side-exchange we either move one container or exchange the location between two containers from the anterior to posterior part of the ship (or vice versa) without changing the side, that can be either the sea or the quay one.

Definition 2. In a *cross-exchange* a container c belonging to C is moved from its current location $l \in A \cap L$ (or, analogously, $l \in A \cap R$) and put in a location, say f, such that $f \in P \cap R(l \in P \cap L)$. f can be either empty or filled with a container $g \in C$; in this last case g is moved from f and put in location l, that is the original location of container c (and vice versa).

    Note that Definition 2 implies that by performing one cross-exchange we either move one container or exchange the location between two containers from the anterior to posterior part of the ship (or vice versa) while changing the side, that is from the sea side to the quay one (or vice versa).

Definition 3. In a *bay-exchange* a whole stack of containers belonging to C is moved from its current bay address $i \in I \cap A$ (or, analogously, $i \in I \cap P$) and located in bay, say e, such that $e \in I \cap P(i \in I \cap A)$ in the same position as far as their row and tier addresses. All rows and tiers at bay e can be empty or filled with a stack of containers; in this last case, such containers are moved from e and located in the same order at bay i.

    Note that Definition 3 implies that by performing one bay-exchange we move either one or two whole stacks of containers and put them, as they are stowed in the current bay, in a different part of the ship, i.e. from the anterior to the posterior part of the ship (and vice versa).

    Of course, any of the above exchange is performed if and only if the new defined location of all containers does not violate constraints (4)–(9). Moreover, we perform the exchanges only among containers having the same destination, that is to say we exchange containers considering only subsets $I_{C_h}, h = 1, \ldots, p$.
    Usually an exchange is performed if the difference between the objective function values of the current and the new solution is in favour of the last one. In our case, we apply a local search not for improving the current solution but for obtaining feasibility in terms of

constraints (4)–(9) and (11)–(12). For this reason we consider as cost θ of an exchange the difference between the related global stability value (15), that is:

$$\theta = \sigma(x^*)' - \sigma(x^*) \tag{16}$$

where $x^{*'}$ denotes the solution obtained from x^* after an exchange of containers. Note that if $\theta < 0$ we have a profitable exchange, since this implies that some unfeasibility has been removed. The cost given in (16) can be in some sense viewed as a penalty function for obtaining feasibility in terms of ship stability as it is proposed in Dubrovsky et al. (2002).

As in any local search algorithm the definition of the neighbourhood and the strategy used during the search are relevant factors. Moreover, the sequence of the defined moves influences the "feasibility" process.

Here above, we have defined three moves (side-exchange, cross-exchange and bay-exchange), respectively, in Definitions 1, 2 and 3. The best sequence of moves that we perform for eliminating unfeasibility is reported in the following c-like procedure, while the scheme of procedures "cross_exchange", "bay_exchange", and "side_exchange" are reported in the Appendix. It can be easily observed that the time complexity of the exchange algorithm is of the order of $\frac{br}{4}$.

Procedure "Checking feasibility"
Begin

   read the solution x^* of model (1)-(10);

   compute the left and right unbalances and the stability violations $\eta(x^*)$, $\sigma_1(x^*)$;

   compute the anterior and posterior unbalances and the stability violations $\chi(x^*)$, $\sigma_2(x^*)$;

   compute the global ship stability $\sigma(x^*) = \sigma_1(x^*) + \sigma_2(x^*)$;

   if $\sigma(x^*) > 0$ **then**   /* the ship stability is violated*/
      begin
         if $\sigma_1(x^*) > 0$ **then** recall **procedure "cross-exchange"** ;
            if feasible == true **then return** "the current solution is feasible";
            if iteration == max_num **then return** "no feasible solution found with respect to constraints (4)-(9),
                                        (11) and (12)"
         if $\sigma_2(x^*) > 0$ **then** recall **procedure "bay-exchange"** ;
            if feasible == true **then return** "the current solution is feasible";
            else
                recall **procedure "side-exchange"** ;
                if feasible == true **then return** "the current solution is feasible";
                else return "no feasible solution found with respect to constraints (4)-(9), (11) and (12)";
      end
   else return "the current solution is feasible";
end

Note that we randomly chose a container for starting the search of a profitable exchange (of course in the Anterior/Posterior or Right/Left part of the ship, in accordance with the existing unfeasibility) and we operate the first profitable exchange found during the search. Since we have defined as a profitable exchange a move such that $\sigma(x^*) < 0$, we accept also a move that reduces $\sigma_1(x^*)$ whilst increases $\sigma_2(x^*)$. The search ends as soon as either a feasible solution is found (i.e. $\sigma_1(x^*) = \sigma_2(x^*) = 0$) or when after a certain number of iterations we are not able to find a change for reducing $\sigma_1(x^*)$ or/and $\sigma_2(x^*)$. In this last case the algorithm returns "No feasible solution found with respect to constraints (4)–(9), (11) and (12)". As we will show in Section 6, in our experiments we obtain a feasible solution in all instances considered.

Table 1 Input data of the sample problem

					Weight			
Destination	n	Size	n	Light	Medium	Heavy	TEUs
1	47	*20*	38	15	20	3	56
		40	9	2	4	3	
2	38	*20*	32	13	18	1	44
		40	6	1	3	2	
3	34	*20*	28	10	16	2	40
		40	6	1	3	2	
			119	42	64	13	140

Containers characteristics

Fig. 2 The bay plan configuration of the sample problem

5. A sample problem

To give an idea of how the proposed three phase algorithm works, let us present a simple case study concerning a 168 TEUs containership, in which we have to stow 119 standard containers, split into 20 and 40 feet. The weight of the containers ranges from 5 to 15 tons (light containers), 15 to 25 tons (medium containers) and more than 25 tons (heavy containers); 3 different ports have to be visited by the ship (see Table 1).

The ship consists of 14 odd bays, namely 1, 3, 5, . . . , 27 (originating seven even bays, namely 2, 6, . . . , 26), 4 rows and 3 tiers (2 in the hold and 1 in the upper deck) and has a maximum capacity of 1800 tons; the maximum horizontal and cross weight tolerance is fixed to 20 and 35 tons, respectively.

By applying the assignment algorithm for the bays presented in Section 2, we obtain subsets I_{C_h}, $h = 1, 2, 3$, given by: $I_{C_1} = \{1, 2, 3, 13, 14, 15, 25, 26, 27\}$, $I_{C_2} = \{5, 6, 7, 17, 18, 19\}$, $I_{C_3} = \{9, 10, 11, 21, 22, 23\}$.

The resulting bay plan configuration is shown in Figure 2. We can see that there is a "two bays" distance between containers having the same destination; in this way the handling time can be possibly reduced by letting the available quay cranes working in parallel.

Then, by using model (1)–(10) we solve the loading problem for each ship partition S_{C_h}, $h = 1, 2, 3$. Note that the formulation of the problem related to the first ship partition S_{C_1}

requires 5076 variables and 2459 constraints, while for S_{C_2} and S_{C_3} we have, respectively, 2736 variables and 1358 constraints, and 2448 variables and 1258 constraints. The objective function values, that is the loading times, are (in minutes): $L^*_{C_1} = 108'\ 6"$, $L^*_{C_2} = 87'\ 48"$, $L^*_{C_3} = 79'\ 6"$. The optimal solutions are obtained on a PC Pentium II by using MPL (Maximal Software, 2000) and Cplex 7.0; the corresponding computational times are $CPU^*_{C_1} = 1'\ 04"$, $CPU^*_{C_2} = 23.94"$, $CPU^*_{C_3} = 17.13"$. The global solution $x^* = \{x^*_{C_1} \cup \ldots x^*_{C_h} \ldots \cup x^*_{C_p}\}$, that gives the final stowage plan of the ship, is reported in Figure 3, where rows are denoted R01, R04, R02, R01 and R03, while the tiers in the hold are Tier 02 and Tier 04 and that in the upper deck is Tier 82.

In the present case x^* is unfeasible since $\eta(x^*) = 25$ and $\chi(x^*) = 100$; consequently, we look for exchanges with the aim of reducing values $\sigma_1(x^*)$ and $\sigma_2(x^*)$, until constraints (11) and (12) are satisfied. We get feasibility by performing one cross-exchange and two side-exchanges, that are depicted in Figure 3 with six arrows. In particular, the first exchange concerns one 20' container that is moved from bay 13 in the left anterior side of the ship to an empty location in bay 25 in the posterior right side; the cost of this change is $\theta = -15$ and hence it is a profitable change. In the following side-exchanges we move two 20' containers in the same side of the ship from the anterior to the posterior part and vice versa, thus removing all the remaining infeasibilities, since $\eta(x^*) = 5$ and $\chi(x^*) = 30$. Note that after this feasibility phase, the objective function value increase of 30", thus resulting in 275' 30".

6. Computational experiments

In this section we present some computational experiments aimed at showing the performance of our algorithm. In particular, our test problems are related to a 198 TEU containership (named Chiwaua), with 11 bays, 4 rows and 5 tiers (3 in the hold and 2 in the upper deck, respectively). Here we test our approach looking for stowage plans of 12 instances, that are reported in Table 2; such instances differ each other for the number of containers to be loaded, ranging from 100 to 148, their size and weight, the number of ports to be visited, that is either 2 or 3, and the number of TEUs to load on board, ranging from 138 to 188. Column "Full" gives the ship occupation level, in percentage, when all containers are loaded; note that we give a 100% occupation level when 188 TEUs are loaded, since, conventionally, 10 TEU locations are operatively always let free for security and possible emergency reasons.

All computational experiments have been performed on a PC Pentium II (clocked at 350 Mhz).

Table 3 gives a picture of how stowage plans for either 2 or 3 ship partitions (instances 11 and 12) are determined by using the proposed three phase algorithm. In particular, the weight distribution in the four main sections of the ship, that is left, right, anterior and posterior, are given. Entries with * refer to instances in which a bay-exchange has been performed after the solution of model (1)–(10).

Note that in some instances, i.e. 8 and 10, the horizontal and cross stability constraints are satisfied by the optimal solutions of model (1)–(10), while after the bay-exchanges only four instances, namely 1, 2, 5 and 12, require further exchanges for getting feasibility.

Table 4 shows the effect of side and cross exchanges on the improvement of the solution in terms of feasibility. Note that the loading time increases only in those instances where we perform a cross-exchange for reducing $\sigma_1(x^*)$ (see rows 1, 2, and 12); in fact, in the case of side-exchanges we move containers and put them in the same rows thus not affecting their loading time.

Table 2 Instances of the containership named Chiwaua

Instance	TEUs	n	Container characteristics																%Full
			Size				Weight						Destination						
			20'	%	40'	%	Light	%	Medium	%	Heavy	%	1	%	2	%	3	%	
1	138	100	62	62,00	38	38,00	46	46,00	50	50,00	4	4,00	47	47,00	53	53,00	0	0	73,40
2	165	120	75	62,50	45	37,50	52	43,33	64	53,33	4	3,33	55	45,83	65	54,17	0	0	87,77
3	170	130	90	69,23	40	30,77	60	46,15	66	50,77	4	3,08	62	47,69	68	52,31	0	0	90,43
4	175	130	85	65,38	45	34,62	58	44,62	68	52,31	4	3,08	62	47,69	68	52,31	0	0	93,09
5	180	140	100	71,43	40	28,57	62	44,29	74	52,86	4	2,86	61	43,57	79	56,43	0	0	95,74
6	180	150	120	80,00	30	20,00	70	46,67	76	50,67	4	2,67	65	43,33	85	56,67	0	0	95,74
7	185	130	75	57,69	55	42,31	60	46,15	66	50,77	4	3,08	62	47,69	68	52,31	0	0	98,40
8	185	140	95	67,86	45	32,14	58	41,43	78	55,71	4	2,86	65	46,43	75	53,57	0	0	98,40
9	188	148	108	72,97	40	27,03	66	44,59	78	52,7	4	2,70	71	47,97	77	52,03	0	0	100,0
10	186	135	84	62,22	51	37,78	59	43,70	72	53,33	4	2,96	60	44,44	75	55,56	0	0	98,94
11	185	140	95	67,86	45	32,14	62	44,29	73	52,14	5	3,57	50	35,71	40	28,57	50	38,46	98,40
12	188	148	108	72,97	40	27,03	68	45,95	76	51,35	4	2,70	50	33,78	50	33,78	48	36,92	100,0

Table 3 Weight configuration and corresponding unfeasibilities of optimal ship partition solutions after bay-exchanges

	CPU*	L*	Weight distribution				
INSTANCE 1							
			Tot.right	Tot.left	bay5/7*	bay13*	bay19/21*
C1	00.54,9	1.48.36	310	325	125	185	325
			Tot.right	Tot.left	bay1/3	bay9/11	bay15/17
C2	00.29,5	2.03.06	380	400	350	210	220
			Tot.right	*Tot.left*	*Tot.ant*	*Tot.post*	
C1+C2	01.24,4	3.51.42	690	725	685	730	
$\sigma_{1,2}$			15			10	
INSTANCE 3							
			Tot.right	Tot.left	bay5/7*	bay13*	bay19/21
C1	01.21,6	2.25,42	365	350	155	285	275
			Tot.right	Tot.left	bay1/3	bay9/11*	bay15/17*
C2	02.01,0	2.40.30	495	510	335	355	315
			Tot.right	*Tot.left*	*Tot.ant*	*Tot.post*	
C1+C2	03.22,6	5.06.12	860	860	845	875	
$\sigma_{1,2}$			0			0	
INSTANCE 5							
			Tot.right	Tot.left	bay5/7	bay13	bay19/21
C1	02.21,5	2.23.06	370	370	305	125	310
			Tot.right	Tot.left	bay1/3	bay9/11*	bay15/17*
C2	1.52,2	3.04.30	455	450	295	280	330
			Tot.right	*Tot.left*	*Tot.ant*	*Tot.post*	
C1+C2	04:13.7	5:27:36	825	820	880	765	
$\sigma_{1,2}$			0			80	
INSTANCE 7							
			Tot.right	Tot.left	bay5/7*	bay13	bay19/21*
C1	02.26,0	2.27.18	360	355	240	110	365
			Tot.right	Tot.left	bay1/3	bay9/11*	bay15/17*
C2	00.42,5	2.38.54	510	495	375	245	385
			Tot.right	*Tot.left*	*Tot.ant*	*Tot.post*	
C1+C2	03.08,5	5.06.12	870	850	860	860	
$\sigma_{1,2}$			0			0	
INSTANCE 9							
			Tot.right	Tot.left	bay5/7	bay13	bay19/21
C1	02.15,3	2.32.48	360	375	165	250	320
			Tot.right	Tot.left	bay1/3	bay9/11	bay15/17
C2	01:30,7	2.43.06	425	425	315	300	235
			Tot.right	*Tot.left*	*Tot.ant*	*Tot.post*	
C1+C2	03:46,0	5.15.54	785	800	780	805	
$\sigma_{1,2}$			0			0	
INSTANCE 11							
			Tot.right	Tot.left	bay9/11*	bay19/21*	
C1	00:28,4	1.56.30	290	300	210	280	
			Tot.right	Tot.left	bay5/7	bay13	
C2	01.14,2	1.34.24	220	235	225	230	
			Tot.right	Tot.left	bay1/3	bay15/17	
C3	02.15,4	1.57.00	270	265	315	220	
			Tot.right	*Tot.left*	*Tot.ant*	*Tot.post*	
C1+C2+C3	03.57,9	5.27.54	780	800	750	730	
$\sigma_{1,2}$			0			0	

(*Continued on the next page*)

Table 3 (*Continued*)

	CPU*	L*	Weight distribution				
INSTANCE 2							
			Tot.right	Tot.left	bay5/7	bay13	bay19/21
C1	00.41,6	2.06.30	360	380	355	120	265
			Tot.right	Tot.left	bay1/3	bay9/11*	bay15/17*
C2	01.20,0	2.30.36	465	480	315	190	440
			Tot.right	*Tot.left*	*Tot.ant*	*Tot.post*	
C1+C2	02.01,6	4.37.06	825	860	860	825	
$\sigma_{1,2}$			15			0	
INSTANCE 4							
			Tot.right	Tot.left	bay5/7*	bay13	bay19/21*
C1	00.47,3	2.23.48	365	380	230	175	340
C2	01.12,0	2.40.30	510	495	375	275	355
			Tot.right	*Tot.left*	*Tot.ant*	*Tot.post*	
C1 + C2	01.59,3	5.04.18	875	875	880	870	
$\sigma_{1,2}$			0			0	
INSTANCE 6							
			Tot.right	Tot.left	bay5/7	bay13	bay19/21
C1	01:59,3	2.33.12	395	380	230	175	340
			Tot.right	Tot.left	bay1/3	bay9/11*	bay15/17*
C2	03.15,4	3.18.48	470	475	340	285	320
C1+C2	05.14,7	5.52.00	865	855	855	835	
$\sigma_{1,2}$			0			0	
INSTANCE 8							
			Tot.right	Tot.left	bay5/7	bay13	bay19/21
C1	00.38.8	2.31.36	390	385	365	150	280
			Tot.right	Tot.left	bay1/3	bay9/11	bay15/17
C2	02.40,2	2.55.24	465	485	280	240	430
			Tot.right	*Tot.left*	*Tot.ant*	*Tot.post*	
C1+C2	03.19,0	5.27.00	855	870	885	860	
$\sigma_{1,2}$			0			0	
INSTANCE 10							
			Tot.right	Tot.left	bay5/7	bay13	bay19/21
C1	02.17,5	2.46.06	390	410	265	180	355
			Tot.right	Tot.left	bay1/3	bay9/11	bay15/17
C2	03.54,3	2.58.18	430	415	255	315	275
			Tot.right	*Tot.left*	*Tot.ant*	*Tot.post*	
C1 + C2	06.11,8	5.44.24	820	825	835	810	
$\sigma_{1,2}$			0			0	
INSTANCE 12							
			Tot.right	Tot.left	bay9/11	bay19/21	
C1	01.30,5	1.56.54	275	255	240	290	
			Tot.right	Tot.left	bay5/7	bay13	
C2	02.38,4	1.56.54	260	270	255	275	
			Tot.right	Tot.left	bay1/3	bay15/17	
C3	02.04,1	1.51.48	255	270	295	230	
			Tot.right	*Tot.left*	*Tot.ant*	*Tot.post*	
C1+C2+C3	06.13,0	5.45.36	515	540	790	795	
$\sigma_{1,2}$			5			0	

Fig. 3 Stowage plan of the sample problem and representation of side and cross exchanges

Table 5 reports the comparison between the optimal solutions obtained by solving the exact 0/1 Linear Programming model for the MBPP reported in Ambrosino et al. (2004) (column LP) and the solutions obtained by using the present algorithmic approach (column BA).

The comparison is based on two main indicators, that is the total loading time L (in hours, minutes and seconds) and the computational time CPU (in minutes and seconds). Note that in the case of our algorithm both L and CPU values related to the final solutions are given by the sum of the corresponding values of each ship partition, such that $L^* = \sum_{h=1}^{p} L_{C_h}$ and $CPU^* = \sum_{h=1}^{p} CPU_{C_h}$.

Table 4 Improvement of the horizontal and cross stability violations after the exchange algorithm

	Loading time (L)								
	(h.mm.ss)			σ_1			σ_2		
Instance	Model (1)–(10)	After bay-exchanges	After cross and side-exchanges	Model (1)–(10)	After bay-exchanges	After cross and side-exchanges	Model (1)–(10)	After bay-exchanges	After cross and side-exchanges
1	3.51.42	3.51.42	3:52.12	15	15	0	320	10	0
2	4.37.06	4.37.06	4.38.54	15	15	0	500	0	0
3	5.06.12	5.06.12	5.06.12	0	0	0	115	0	0
4	5.04.18	5.04.18	5.04.18	0	0	0	355	0	0
5	5.27.36	5.27.36	5.27.36	0	0	0	180	80	0
6	5.52.00	5.52.00	5.52.00	0	0	0	0	0	0
7	5.06.12	5.06.12	5.06.12	0	0	0	495	0	0
8	5.27.00	5.27.00	5.27.00	0	0	0	0	0	0
9	5.15.54	5.15.54	5.15.54	0	0	0	120	0	0
10	5.44.24	5.44.24	5.44.24	0	0	0	125	0	0
11	5.27.54	5.27.54	5.27.54	0	0	0	0	0	0
12	5.45.36	5.45.36	5.46.06	5	5	0	0	0	0
Average	5.13.50	5.13.50	5.14.04	3	3	0	184	8	0

Table 5 Comparison of the loading time and the computational time between our solutions and the optimal ones

	Loading time (L) (h.mm.ss)			CPU (mm.ss,0)		
Instance	LP	BA	$\Delta\%$	LP	BA	$\Delta\%$
1	3.46.54	3.52.12	2,34	03.25,0	01.34,8	53,76
2	4.32.36	4.38.54	2,31	08.28,4	02.11,9	74,06
3	5.01.48	5.06.12	1,46	10.32,4	03.33,1	66,30
4	5.00.36	5.04.18	1,23	03.33,7	02.09,8	39,26
5	5.24.24	5.27.36	0,99	10.08,2	04.24,0	56,59
6	5.48.12	5.52.00	1,09	14.27,5	05.25,0	62,54
7	5.03.06	5.06.12	1,02	11.02,0	03.19,0	69,94
8	5.24.00	5.27.00	0,93	15.38,3	03.29,1	77,72
9	5.13.18	5.15.54	0,83	05.52,8	03.56,1	33,08
10	5.43.48	5.44.24	0,17	13.32,1	06.21,9	52,98
11	5.25.12	5.27.54	0,83	14.53,6	04.08,3	72,21
12	5.45.36	5.46.06	0,14	13.17,6	06.23,2	51,96
Average	5.10.48	5.14.04	1,05	10.24,3	03.54,7	59,20

Table 6 Main information and results about a real scale instance

				Weight				
Destination n		Size n		Light	Medium	Heavy	TEUs	
1	100	*20*	70	30	20	20	130	
		40	30	10	10	10		
2	120	*20*	90	40	20	30	150	
		40	30	15	10	5		
3	80	*20*	60	20	20	20	100	
		40	20	5	5	10		
	300		300	42	64	13	380	

Ship Characteristics				LP Model				BA Algorithm	
						L	CPU	L	CPU
Bays	Rows	Tiers	TEUs	Variables	Contraints	(hh.mm.ss)	(hh.mm.ss,0)	(hh.mm.ss)	(hh.mm.ss,0)
17	6	6	612	356.400	4.257	–	> 60.00.00,0	11.15.43	00.30.40,3

See the goodness of our solutions that are on the average about 1.05% greater than the optimal values and, in the worst case, only 2.34%. Moreover, note the impressive reduction of the CPU time of our approach, that is up to 59.20%. Even if in absolute terms the above CPU time reduction is not significant, when considering larger instances it becomes noticeable. A large amount of numerical experiments have been carried out in this direction with various patterns of containers and different sizes of ships; unfortunately, we were not able to find optimal values *LP* as for the instances given in Table 5. To get an idea of the explosive CPU time required for solving the MBPP up to optimality Table 6 reports some information about a large real case instance for which we were not able to find any integer solution in more than 60 hours of CPU time; of course for this instance we cannot prove the goodness of the solution but starting from the results given in Table 5 we believe that the optimality gap is very tight.

7. Conclusions

In this paper we have presented a three phase algorithm for the MBPP, that is based on a partitioning procedure that splits the ship into different portions and assigns them to containers on the basis of their destination. The proposed solution method has very good performances in terms of both solution quality and computational time. Looking at the given results, we believe that the proposed approach is particularly suitable for determining stowage plans of large size containerships, also considering the possibility of exploiting the potential of commercial software, as Cplex, for solving up to the optimality single bay partitions of the ship. Moreover, our algorithm enables the loading operations of each portion of the ship to be performed in parallel thus minimising the loading time of the containership and hence improving the competitiveness of maritime terminals.

Appendix

Procedure "cross-exchange"   /* apply when $\sigma_1(x^*) > 0$, $\sigma_2(x^*) \geq 0$ */
begin
   /* initialisation */
   $WLS = \sum\limits_{i,j \in L, k} \sum\limits_{c} w_c x^*_{ijkc}$;   /* total weight in left locations */

   $WRS = \sum\limits_{i,j \in R, k} \sum\limits_{c} w_c x^*_{ijkc}$;   /* total weight in right locations */

   feasible = false;   /* say if a feasible solution is found */
   iteration = 0;   /* count the # of iteration for finding a profitable exchange */
   /* compute the side unbalances and assign the correct value to variable S for searching the change */
   if $WLS > WRS$ **then** $S = L$ **else** $S = R$;
   do
      iteration = ++iteration;
      choose B belonging to A or P;
      choose h belonging to set{ 1,2,.....p };
      choose a non-empty location l_1 such that $i_1 \in I_{C_h} \cap B, j_1 \in S$, $k_1 \in K$;

      /* c_{l_1} is the container assigned to it, its weight and its destination are W[c_{l_1}] , D[c_{l_1}] */

      AL = {l_{ijk}: i$\in I_{C_h} \cap (I \backslash B), j \in J \backslash S$, k$\in$K }; /* set of available location for looking for a change */

      exchange = false;   /* say if a feasible improvement exchange is found */
      while (exchange == false **or** AL $\neq \varnothing$)
          begin
           choose a location l_2 from AL;
          if   W[c_{l_1}]$>$W[c_{l_2}] and D[c_{l_1}]$==$D[c_{l_2}]   **then**
             begin /* Check feasibility for location l_2 */
                if constraints (4)-(9) are satisfied for the new location of c_{l_1} in l_2 **then**
                    if location l_2 is empty **then**
                       c_{l_1} is assigned to l_2 and location l_1 become empty;   / * update the solution *.

                       exchange = true, iteration = 0, update $\sigma_1(x^*)$, $\sigma_2(x^*)$;
                    else   /* Check feasibility for location l_1 */
                       if constraints (4)-(9) are satisfied for the new location of c_{l_2} in l_1 **then**

                          c_{l_1} is assigned to l_2 , c_{l_2} is assigned to l_1 ;

                          exchange = true, iteration = 0, update $\sigma_1(x^*)$, $\sigma_2(x^*)$;
                       else   AL=AL \{l_2};
                    else AL=AL \{l_2};
             end
          else AL=AL \{l_2};
          end
   while ($\sigma_1(x^*)$ $>$0 or iteration == max_num);

   if $\sigma_2(x^*)$ $== 0$ **then** feasible = true;

   return iteration, feasible, $\sigma_1(x^*)$, $\sigma_2(x^*)$;
end

Procedure "side-exchange"   /* apply when $\sigma_2(x^*) > 0$, $\sigma_1(x^*) = 0$ */
begin
    /* initialisation */

$$WPB = \sum_{i \in P, j, k} \sum_c w_c x^*_{ijkc} \qquad \text{/* total weight in posterior bays */}$$

$$WAB = \sum_{i \in A, j, k} \sum_c w_c x^*_{ijkc} \qquad \text{/* total weight in anterior bays */}$$

feasible = false;   /* say if a feasible solution is found */
iteration = 0;   /* count the # of iteration for finding a profitable exchange */
 /* compute the side unbalances and assign the correct value to variable B for searching the change */
if $WPB > WAB$ **then** $B = P$ **else** $B = A;$
do
  iteration = ++iteration
  choose J belonging to L or R ;
  choose h belonging to set{ $1,2,\dots.p$ };
  choose a non-empty location l_1 such that $i_1 \in I_{C_h} \cap B, j_1 \in J,\ k_1 \in K;$

  /* c_{l_1} is the container assigned to it, its weight and its destination are $W[c_{l_1}]$, $D[c_{l_1}]$ */

  AL = {l_{ijk}: $i \in I_{C_h} \cap (I \backslash B), j \in J,\ k \in K$ };   /* set of available location for looking for a change */

  exchange = false;   /* say if a feasible improvement exchange is found */
  while (exchange = false **or** AL $\neq \varnothing$)
    begin
      choose a location l_2 from AL;
      if   W[c_{l_1}]>W[c_{l_2}] and D[c_{l_1}]==D[c_{l_2}] **then**
        begin /* Check feasibility for location l_2 */
          if constraints (4)-(9) are satisfied for the new location of c_{l_1} in l_2 **then**
            if location l_2 is empty **then**
              c_{l_1} is assigned to l_2 , location l_1 become empty; / * update the solution */

              exchange = true, iteration = 0, update $\sigma_2(x^*)$ **;**
            else   /* Check feasibility for location l_1 */
              if constraints (4)-(9) are satisfied for the new location of c_{l_2} in l_1 **then**

                c_{l_1} is assigned to l_2 , c_{l_2} is assigned to l_1 ; / * update the solution */

                exchange = true, iteration = 0, update $\sigma_2(x^*)$;
              else   AL=AL \{l_2};
          else AL=AL \{l_2};
        end
        else AL=AL \{l_2};
      end
  while ($\sigma_2(x^*) > 0$ or iteration = max_num);

 if $\sigma_2(x^*) = 0$ **then** feasible = true;

 return iteration**,** feasible, $\sigma_2(x^*)$;
end

Procedure "bay-exchange"   /* apply when $\sigma_2(x^*) > 0$, $\sigma_1(x^*) = 0$ */
begin
  /* initialisation */
$$WPB = \sum_{i \in P, j, k} \sum_{c} w_c x^*_{ijkc} \qquad /* \text{ total weight in posterior bays } */$$

$$WAB = \sum_{i \in A, j, k} \sum_{c} w_c x^*_{ijkc} \qquad /* \text{ total weight in anterior bays } */$$

  feasible = false;   /* say if a feasible solution is found */
  iteration = 0;   /* count the # of iteration for finding a profitable exchange */
   /* compute the side unbalances and assign the correct value to variable B for searching the change */
  if $WPB > WAB$ **then** $B = P$ **else** $B = A;$
  do
   bay = false;   /* say if a bay in a given destination is found for searching an exchange */
   iteration = ++iteration;
   exchange = false;   /* say if a feasible improvement exchange is found */
   while (bay == false or $D \neq \varnothing$)
      choose h belonging to set D={ 1,2,.....p };
       if $I_{C_h} \cap B = \varnothing$ **then** D = D\{h};
       else bay = true;
    choose a non-empty bay b_1 such that $i_l \in I_{C_h} \cap B;$

    /* C_{b_1} are the containers assigned to it, W[C_{b_1}] is the total weight of them */

    AB = $I_{C_h} \cap (I \backslash B);$ /* set of available bays for looking for a change */

   while (exchange = =false or AB $\neq \varnothing$)
      begin
          choose a bay b_2 from AB;
       if   W[C_{b_1}]$>$W[C_{b_2}]   **then**
            begin /* update the solution */
                 if bay b_2 is empty **then**
                       C_{b_1} are assigned to b_2 , bay b_1 become empty;
                 else
                       C_{b_1} are assigned to b_2 , C_{b_2} are assigned to $b_1;$

                 exchange = true, iteration = 0, update $\sigma_2(x^*);$
            end
          else AB=AB $\backslash \{b_2\};$
      end
  while ($\sigma_2(x^*) > 0$ or iteration= = max_num);

  if $\sigma_2(x^*) == 0$ **then**   feasible = true;

  return iteration, feasible, $\sigma_2(x^*);$
end

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